

The Behavior of the Lubricant Film to Dynamic Stress at a Radial Bearing with HD Lubrication

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Abstract: *The researches regarding the behavior of HD radial bearings in the conditions of operation with shocks and vibrations, are performed considering known the functional characteristics of the bearing in static regime. In the presented experimental research, the functional characteristics of the bearing in static regime are considered known, the measurements focusing on determining the minimum electrical resistance of the lubricant film, which estimates the minimum thickness of lubricant in the bearing.*

Keywords: *film resistivity, lubricant thickness, bearing.*

1 INTRODUCTION

It is found that depending on the loading, speed and dynamic viscosity of the lubricant, the minimum thickness of the lubricant film and the value of the friction coefficient can be changed [4], [5]. In the experimental research was used, an additive mineral oil for bearings, type LA 32, STR 5152-89, viscosity class ISO VG 32.

Due to the short time in which the dynamic loading takes place, it can be stated that the predominant phenomenon of achieving the bearing capacity of these bearings is the effect of expelling the lubricant from the gap.

2 EXPERIMENTAL DEVICES AND ACQUISITION CHAINS

The lubricant film resistivity, it determined through the achievement of a circuit between spindle and bushing which include a standard resistance $R_{12} = 49 \text{ K}\Omega$ (figure 1) [2], [3], [7]. The radial bearing spindle has a nominal diameter $D = 60 \text{ mm}$, made of 18MoCr10 material, the bronze bearing in the composition, 88% Sn, 8% Sb, 4% Cu, has a width $L = 30 \text{ mm}$, is presented in figure 2. The variation of the input speed is made with the help of the gearbox, which ensures the speeds of 960, 600 and 370 rpm. The static bearing loading system allows loading with forces $G_1 = 2250 \text{ N}$, respectively $G_2 = 4500 \text{ N}$. The dynamic bearing loading system allows loading with forces $F_1 = 1665 \text{ N}$ ($H=5 \text{ cm}$), $F_2 = 2356 \text{ N}$ ($H=20 \text{ cm}$), $F_3 = 3332.5 \text{ N}$ ($H=40 \text{ cm}$).

All the tests were made at a 40°C of the lubricant, being constant, pressure distribution p_{in} having the following values, from 0,5 bar to 10 bar [1], [6].

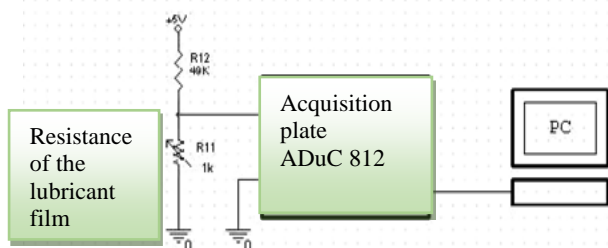


Fig. 1. Measuring the resistance of the lubricant film

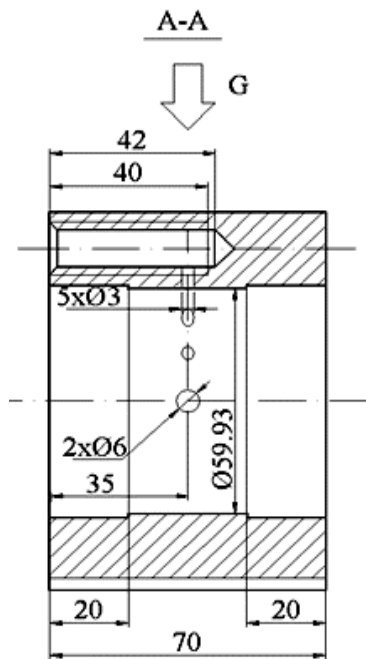
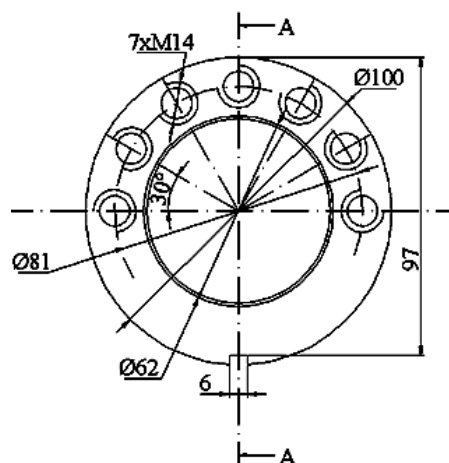


Fig. 2. The HD radial bearing



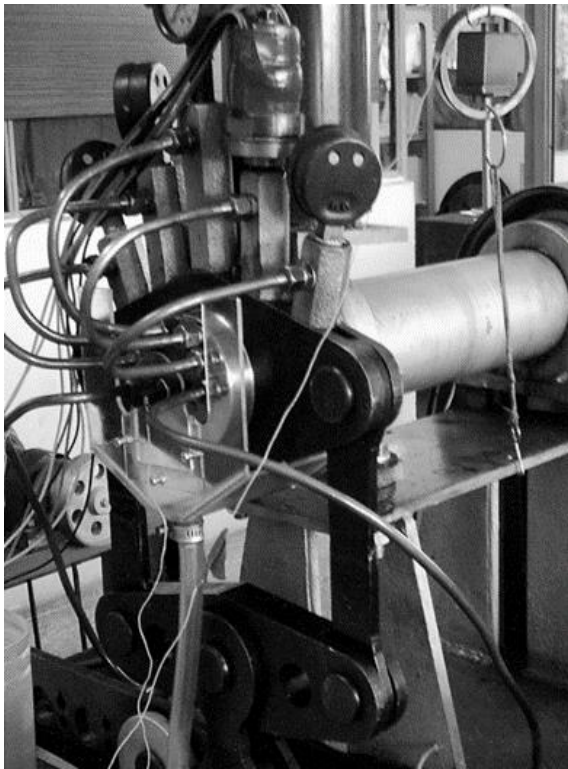


Fig. 3. The testing experimental devices

3. EXPERIMENTAL RESULTS

For the study it was used the experimental testing device of the radial bearings belonging to Technical University of Cluj-Napoca, North University Center of Baia Mare, Faculty of Engineering, Industrial Systems and Technology Management Department, (figure 3).

Influence of speed and supply pressure on electrical resistance minimum lubricant film, the dynamic and static charging conditions at different spindle's rotations are presented in figure 4 for $n=370$ rot/min, $p_{in}=0,5$ bar, figure 5 for $n=600$ rot/min, $p_{in}=1,5$ bar and figure 6 for $n=960$ rot/min, $p_{in}=8$ bar [1].

Notations used:

L- length of bearing (m); G- static loading (N); p- pressure (Pa); F- dynamically loading (N); h- fluid film thickness (m); D- bearing shaft diameter (m); H - weight launching height (m); n – the rotational speed.

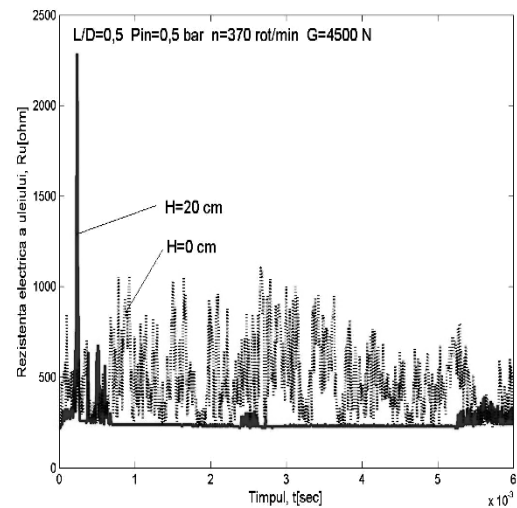
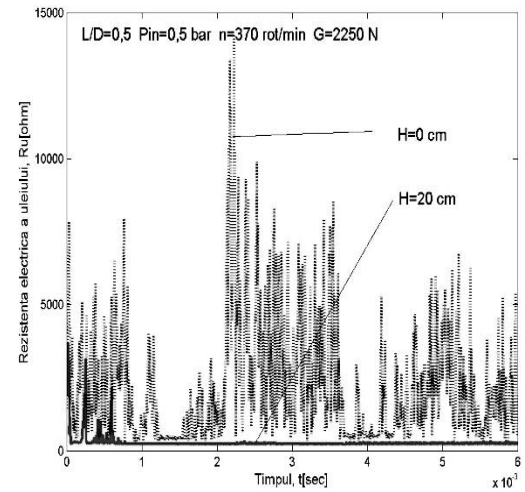
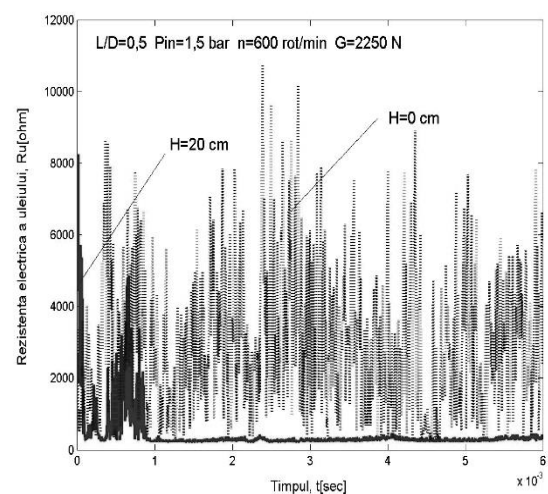


Fig. 4. The electrical resistance of the lubricant film for $p_{in}=0,5$ bar, $n=370$ rot/min, in relation to the dynamic and static charging of the bearing



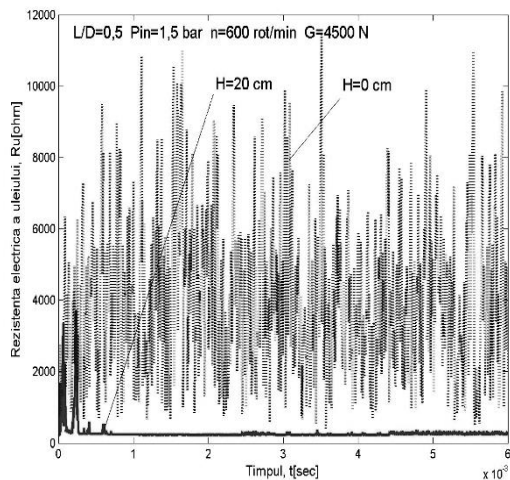


Fig. 5. The electrical resistance of the lubricant film for $p_{in}=1,5$ bar, $n=600$ rot/min, in relation to the dynamic and static charging of the bearing

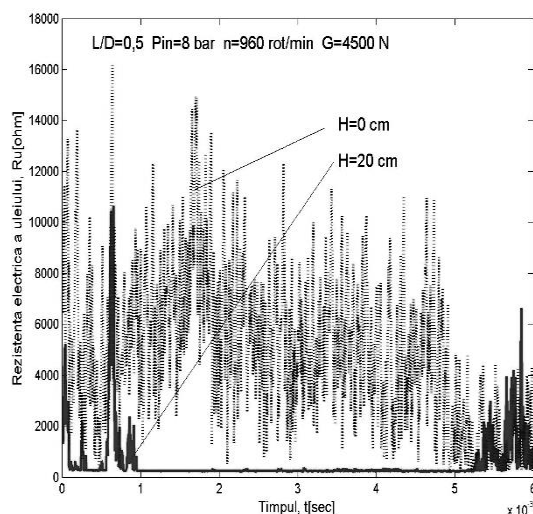
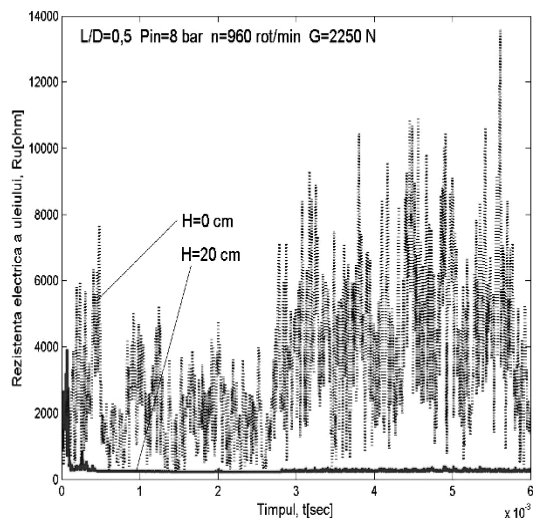


Fig. 6. The electrical resistance of the lubricant film for $p_{in}=8$ bar, $n=960$ rot/min, in relation to the dynamic and static charging of the bearing

4. CONCLUSIONS

The following observations can be stated:

- the higher the dynamic shock load, the lower the electrical resistance of the film, the decrease being made progressively with the increase of the load;
- drastic reduction of the thickness of the lubricant film in the area corresponding to the moment of shock;
- for $n = 600$ rot / min, the decrease of the average value of the resistance of the lubricant film in relation to the value from the static regime is between 9.93 - 12.11 times, depending on the static load;
- at the spindle speed of 960 rot / min, the decrease of the average value of the resistance of the lubricant film in relation to the value in the static regime is between 12.87 - 22.67 times, depending on the applied static load;
- in all situations studied, from a theoretical point of view, at high dynamic loads, over 2000 N, the minimum thickness of the lubricant film falls below the minimum allowable value of $5 \mu\text{m}$, the results being in full accordance with experimental research, where the value of electrical resistance of the lubricant film suddenly decreases to a minimum value (275Ω , penetration value of the lubricant film and implicitly metallic contact);
- both from a theoretical and experimental point of view, the decrease of the minimum thickness of the lubricant film is noticed with the increase of the static and dynamic load of the radial bearing;
- the supply pressure does not significantly influence the minimum thickness of the lubricant film determined both theoretically and experimentally;
- the increase of the spindle speed leads to the increase of the minimum lubricant thickness, with favorable implications on the radial bearing capacity.

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