

DYNAMICS BRAKING OF THE LIFT

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Abstract: In this paper it is presented an approaching method of the dynamic process regarding to the lift mechanic brake with friction wheel.

Key – words: lift, brake moment, generalize co-ordinates, generalize speeds, kinetic energy, and potential energy.

1. INTRODUCTION

For the theoretical establishment of the dynamic characteristics of the lift's elastic system at brake, it is presented the gravel scheme in figure 1.

When the wording problem take place (when the gravel algorithm is elaborated) there are accepted the next assumptions:[1][2][4]

- the actuation engine is stopped, in conclusion the moment engine is null.
- the reduced mass at the periphery of brake rim for all elements which execute a rotation movement it's considered as an inertia moment reduced I_{np} – to he drum's axis of all the elements in the rotating movement (of the engine, the redactor, the ropes , the pulleys).
- because the moment of braking apply directly on the friction wheel, the rigid/stern of branches cables and the rigid of the action system have a considerable influence on the mechanic system

In the figure 1:

- m_1, m_2 means the cabin and the counterweight's masses;

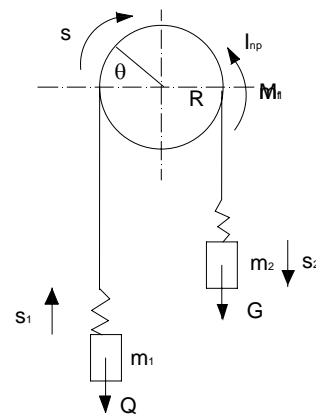


Fig. 2.

- s_1, s_2 și s reprezintă mișcările maselor și mișcarea adecvată a unghiului de rotație θ al roții de fricțiune în momentul aplicării momentului de frânare până când mișcarea se oprește;
- c_1 și c_2 coeficienții de rigiditate ai celor două ramuri de cablu.

2. MATHEMATIC MODEL

Ecuația mișcării liftului, în timpul frânării, este scrisă sub forma ecuației generale, cu ajutorul ecuației Lagrange [3]

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{\rho}_i} \right) - \frac{\partial T}{\partial \rho_i} = - \frac{\partial \Pi}{\partial \rho_i} - \frac{\partial D}{\partial \rho_i} + Q_i(t), \quad (1)$$

în care:

- T - energia cinetică a sistemului mecanic;
- Π - energia potențială;
- ρ_i - coordonate generalizate;
- D - funcția de disipare;
- $Q_i(t)$ - forțe generalizate.

În cazul nostru considerăm $q_1 = s$, $q_2 = s_1$, $q_3 = s_2$, iar forțele generalizate sunt:

$$\begin{cases} Q_1(t) = Q - G + F_f(t) \\ Q_2(t) = -Q \\ Q_3(t) = G \end{cases} \quad (2)$$

În care F_f este rezultatul forțelor de frânare, Q forțele greutății cabinei, G forțele greutății contraponderului.

Forțele generalizate sunt: $\frac{ds}{dt} = \dot{q}_1$, $\frac{ds_1}{dt} = \dot{q}_2$, $\frac{ds_2}{dt} = \dot{q}_3$.

- $\dot{\theta} = \dot{q}_3$ - viteza unghiulară;
- $\frac{ds}{dt}$ - viteza cabinei;
- $\frac{ds_1}{dt}$ - viteza contraponderului.

Energia cinetică este scrisă sub forma:

$$T = \frac{m_{np}}{2} \cdot \dot{q}_1^2 + \frac{m_1}{2} \cdot \dot{q}_2^2 + \frac{m_2}{2} \cdot \dot{q}_3^2, \quad (3)$$

We obtain the partial derivative:

$$\frac{\partial T}{\partial \dot{q}_1} = I_{np} \cdot \dot{q}_1, \quad (4)$$

$$\frac{\partial T}{\partial \dot{q}_2} = m_1 \cdot \dot{q}_2, \quad (5)$$

$$\frac{\partial T}{\partial \dot{q}_3} = m_2 \cdot \dot{q}_3 \quad (6)$$

and we have

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_1} \right) = I_{np} \cdot \ddot{q}_1, \quad (7)$$

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_2} \right) = m_1 \cdot \ddot{q}_2, \quad (8)$$

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_3} \right) = m_2 \cdot \ddot{q}_3. \quad (9)$$

Potential energy is written under the form:

$$\Pi = \frac{1}{2} (q_1 - q_2)^2 \cdot c_1 + \frac{1}{2} (q_3 - q_1)^2 \cdot c_2 \quad (10)$$

We obtain the partial derivative:

$$\frac{\partial \Pi}{\partial q_1} = (q_1 - q_2) \cdot c_1 - (q_3 - q_1) \cdot c_2 \quad (11)$$

$$\frac{\partial \Pi}{\partial q_2} = -(q_1 - q_2) \cdot c_1 \quad (12)$$

$$\frac{\partial \Pi}{\partial q_3} = (q_3 - q_1) \cdot c_2 \quad (13)$$

We consider that the external forces are proportional with the speed than the dissipative function has this form [3]:

$$D = \frac{1}{2} k_1 \cdot \dot{q}_2^2 + \frac{1}{2} k_2 \cdot \dot{q}_3^2, \quad (14)$$

In which k_1 and k_2 are dissipation coefficients.

The dissipation function has the partial derivative:

$$\frac{\partial D}{\partial q_1} = 0 \quad (15)$$

$$\frac{\partial D}{\partial q_2} = k_1 \cdot \dot{q}_2 \cdot \ddot{q}_2 \quad (16)$$

$$\frac{\partial D}{\partial q_3} = k_2 \cdot \dot{q}_3 \cdot \ddot{q}_3 \quad (17)$$

Replacing the value of T, Π, D, in the equation (1) and in condition bases (2) results the following system of the differentiated equation:

$$\begin{cases} m_{np} \left(\ddot{q}_1 - \dot{q}_1 \right) = (q_1 - q_2) \cdot c_1 - (q_3 - q_1) \cdot c_2 + Q - G + F_f(t) \\ m_1 \left(\ddot{q}_2 - \dot{q}_2 \right) = -(q_1 - q_2) \cdot c_1 - k_1 \dot{q}_3 \ddot{q}_2 - Q \\ m_2 \left(\ddot{q}_3 - \dot{q}_3 \right) = (q_3 - q_1) \cdot c_2 - k_2 \dot{q}_3 \ddot{q}_3 + G \end{cases} \quad (18)$$

The system can be solved trough numbering methods

CONCLUSIONS

Replacing in the system (18) the numbering values for the masses, for the coefficients and for the braking moment (for concrete cases of working), it's possible to determine the generalized coordinates which are the movements s_1 , s_2 end s . Knowing these movements is very important to achieve the position of the cabin at the loading and unloading platform level.

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